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**TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)
CONCERNING A FILING UNDER 35 U.S.C. 371**

ATTORNEY'S DOCKET NUMBER

USPL-64

U.S. APPLICATION NO. (if known, see 37 CFR 1.5)

09/554135INTERNATIONAL APPLICATION NO.
PCT/US98/23937INTERNATIONAL FILING DATE
10 November 1998 (10.11.98)PRIORITY DATE CLAIMED
13 November 1997 (13.11.97)

TITLE OF INVENTION

**WIDE FIELD OF VIEW PROJECTION LENSES FOR COMPACT PROJECTION LENS
SYSTEMS EMPLOYING PIXELIZED PANELS**

APPLICANT(S) FOR DO/EO/US MOSKOVICH, Jacob

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☐ This express request to begin national examination procedures (35 U.S.C. 371(f) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT articles 22 and 39(1).
4. ☒ A proper Demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date.
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2))
 - a. ☐ is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ has been transmitted by the International Bureau.
 - c. ☒ is not required, as the application was filed in the United States Receiving Office (RO/US)
6. ☒ A translation of the International Application into English (35 U.S.C. 371(c)(2)).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)).
 - a. ☐ are transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ have been transmitted by the International Bureau.
 - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - d. ☒ have not been made and will not be made.
8. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. ☒ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
10. ☐ A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11. to 16. below concern document(s) or information included:

11. ☐ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☒ A **FIRST** preliminary amendment.
☐ A **SECOND** or **SUBSEQUENT** preliminary amendment.
14. ☐ A substitute specification.
15. ☐ A change of power of attorney and/or address letter.
16. ☒ Other items or information:
(see Express Mail Information)

U.S. APPLICATION NO. (if known, see 37 CFR 1.5)

INTERNATIONAL APPLICATION NO.

ATTORNEY'S DOCKET NUMBER

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USPL-64 PCT

- 17.
- ☒
- The following fees are submitted:

BASIC NATIONAL FEE (37 CFR 1.492 (a) (1)-(5)):

Neither international preliminary examination fee (37 CFR 1.482)
nor international search fee (37 CFR 1.445(a)(2) paid to USPTO
and International Search Report not prepared by the EPO or JPO \$970.00

International preliminary examination fee (37 CFR 1.482) not paid to
USPTO but International Search Report prepared by the EPO or JPO \$840.00

International preliminary examination fee (37 CFR 1.482) not paid to USPTO
but international search fee (37 CFR 1.445(a)(2) paid to USPTO \$760.00

International preliminary examination fee paid to USPTO (37 CFR 1.482)
but all claims did not satisfy provisions of PCT Article 33(1)-(4) \$670.00

International preliminary examination fee paid to USPTO (37 CFR 1.482)
and all claims satisfied provisions of PCT Article 33(1)-(4) \$96.00

ENTER APPROPRIATE BASIC FEE AMOUNT =**CALCULATIONS** PTO USE ONLY

Surcharge of \$130.00 for furnishing the oath or declaration later than ☐ 20 ☐ 30
months from the earliest claimed priority date (37 CFR 1.492(e)).

CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE
Total claims	27 - 20 = 7		X \$18.00
Independent claims	2 - 3 = 0		X \$78.00
MULTIPLE DEPENDENT CLAIM(S) (if applicable)			+ \$260.00

TOTAL OF ABOVE CALCULATIONS =

Reduction by 1/2 for filing by small entity, if applicable. A Small Entity Statement
must also be filed (Note 37 CFR 1.9, 1.27, 1.28).

SUBTOTAL =

Processing fee of \$130.00 for furnishing the English translation later than ☐ 20 ☐ 30
months from the earliest claimed priority date (37 CFR 1.492(f)).

TOTAL NATIONAL FEE =

Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be
accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property +

TOTAL FEES ENCLOSED =

Amount to be: refunded	\$
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- a. ☒ A check in the amount of \$482.00 to cover the above fees is enclosed.
- b. ☐ Please charge my Deposit Account No. 11-1158 in the amount of \$_____ to cover the above fees.
- c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required by this paper, or credit any overpayment to Deposit Account No. 11-1158. A duplicate copy of this sheet is enclosed

NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.

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International Appl. No. : PCT/US98/23937
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Title of Invention : WIDE FIELD OF VIEW PROJECTION
LENSES FOR COMPACT PROJECTION
LENS SYSTEMS EMPLOYING PIXELIZED
PANELS
U.S. Serial No. : Not Yet Assigned
Applicant (U.S.) : Jacob Moskovich

BOX PCT
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WASHINGTON, D.C. 20231
ATTENTION: DO/EO/US

PRELIMINARY AMENDMENT

Prior to its initial examination, please insert before the first line of the specification:

--CROSS REFERENCE TO RELATED APPLICATIONS

This is the U.S. national phase of International Application No. PCT/US98/23937 filed November 10, 1998. This application claims the benefit under 35 USC §119(e) of U.S. Provisional Application No. 60/065,308 filed November 13, 1997.--

Respectfully submitted,

Date: 10 May 2000

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5 WIDE FIELD OF VIEW PROJECTION LENSES FOR COMPACT
 PROJECTION LENS SYSTEMS EMPLOYING PIXELIZED PANELS

FIELD OF THE INVENTION

 This invention relates to projection lenses and, in particular, to
10 projection lenses which can be used, inter alia, to form an image of an object
 composed of pixels, e.g., a LCD.

BACKGROUND OF THE INVENTION

 Projection lens systems (also referred to herein as "projection
 systems") are used to form an image of an object on a viewing screen. The
15 basic structure of such a system is shown in Figure 6, wherein 10 is a light
 source (e.g., a tungsten-halogen lamp), 12 is illumination optics which
 forms an image of the light source (hereinafter referred to as the "output" of
 the illumination system), 14 is the object which is to be projected (e.g., a
 LCD matrix of on and off pixels), and 13 is a projection lens, composed of
20 multiple lens elements, which forms an enlarged image of object 14 on
 viewing screen 16. The system can also include a field lens, e.g., a Fresnel
 lens, in the vicinity of the pixelized panel to appropriately locate the exit
 pupil of the illumination system.

 For front projection systems, the viewer will be on the left side of
25 screen 16 in Figure 6, while for rear projection systems, the viewer will be
 on the right side of the screen. For rear projection systems which are to be
 housed in a single cabinet, a mirror is often used to fold the optical path
 and thus reduce the system's overall size. The projection lenses of the
 present invention are particularly well suited for use in rear projection
30 systems, but can be used in front projection systems if desired.

 Projection lens systems in which the object is a pixelized panel are

used in a variety of applications, including data display systems. Such projection lens systems preferably employ a single projection lens which forms an image of, for example, a single panel having red, green, and blue pixels. In some cases, e.g., large image rear projection systems, multiple
5 panels and multiple projection lenses are used, with each panel/projection lens combination producing a portion of the overall image.

Pixelized panels, specifically, LCD panels, come in various sizes depending upon the type of projection system in which they are to be used. Large LCD panels, e.g., panels having a diagonal of about 12.5 inches
10 (about 320 millimeters), can be effectively employed in producing high resolution color images since such panels can have a high pixel count while still maintaining a pixel size which is large enough for reliable manufacture. In this regard, it should be noted that for a full color image from a single LCD panel, the number of pixels needed is three times that
15 required for a monochrome image, thus making for small pixel sizes unless large LCD panels are used.

There exists a need in the art for a projection lens for use with a large pixelized panel which simultaneously has at least the following properties: (1) a wide field of view, i.e., a relatively short focal length; (2)
20 the ability to operate at various magnifications while maintaining a high level of aberration correction; (3) a relatively small size, including a relatively small number of lens elements, a relatively small barrel length, and a relatively small maximum lens diameter; (4) a high level of color correction; (5) low distortion; and (6) low sensitivity to temperature
25 changes.

A wide field of view allows the overall projection lens system to be compact which is highly desirable for installations where space is at a premium. In particular, compactness minimizes the size and thus cost of the cabinetry needed to house the projection system and facilities packing
30 and shipping of the finished system to the user.

A projection lens which can efficiently operate at various

magnifications is desirable since it allows the projection system to be used with screens of different sizes without the need to change any of the components of the system. Only the object and image conjugates need to be changed which can be readily accomplished by moving the lens relative to the pixelized panel. The challenge, of course, is to provide a high level of aberration correction throughout the operative range of magnifications.

A relatively small projection lens is desirable from a cost, weight, and size point of view. Large numbers of lens elements and elements having large diameters consume more raw materials, weigh more, and are more expensive to build and mount. Long barrel lengths normally increase the overall size of the projection system, which again leads to increased cost and weight. Accordingly, a lens with a minimum number of relatively small lens elements, located relatively close to one another, is desired.

A high level of color correction is important because color aberrations can be easily seen in the image of a pixelized panel as a smudging of a pixel or, in extreme cases, the complete dropping of a pixel from the image. These problems are typically most severe at the edges of the field. In general terms, the color correction, as measured at the pixelized panel, should be better than about a pixel and, preferably, better than about a half a pixel to avoid these problems.

All of the chromatic aberrations of the system need to be addressed, with lateral color, chromatic variation of coma, and chromatic aberration of astigmatism typically being most challenging. Lateral color, i.e., the variation of magnification with color, is particularly troublesome since it manifests itself as a decrease in contrast, especially at the edges of the field. In extreme cases, a rainbow effect in the region of the full field can be seen.

In projection systems employing cathode ray tubes (CRTs) a small amount of (residual) lateral color can be compensated for electronically by, for example, reducing the size of the image produced on the face of the red CRT relative to that produced on the blue CRT. With a pixelized panel,

however, such an accommodation cannot be performed because the image is digitized and thus a smooth adjustment in size across the full field of view is not possible. A higher level of lateral color correction is thus needed from the projection lens.

5 The use of a pixelized panel to display data leads to stringent requirements regarding the correction of distortion. This is so because good image quality is required even at the extreme points of the field of view of the lens when viewing data. As will be evident, an undistorted image of a displayed number or letter is just as important at the edge of the field as it
10 is at the center.

 In order to produce an image of sufficient brightness, a substantial amount of light must pass through the projection lens. As a result, a significant temperature difference normally exists between room temperature and the lens' operating temperature. In addition, the lens
15 needs to be able to operate under a variety of environmental conditions. For example, projection lens systems are often mounted to the ceiling of a room, which may comprise the roof of a building where the ambient temperature can be substantially above 40°C. To address these effects, a projection lens whose optical properties are relatively insensitive to
20 temperature changes is needed.

 One way to address the temperature sensitivity problem is to use lens elements composed of glass. Compared to plastic, the radii of curvature and the index of refraction of a glass element generally change less than those of a plastic element. However, glass elements are generally
25 more expensive than plastic elements, especially if aspherical surfaces are needed for aberration control. As described below, plastic elements can be used and temperature insensitivity still achieved provided the powers and locations of the plastic elements are properly chosen.

 The projection lenses described below achieve all of the above
30 requirements and can be successfully used in producing relatively low cost projection lens systems capable of forming a high quality color image of a

pixelized panel on a viewing screen. In particular, as illustrated by the examples presented below, the lenses of the invention can, for example, have a field of view of up to $\pm 45^\circ$, can operate at $f/4$, and can have a magnification range of 5.5X to 9.6X.

5 DESCRIPTION OF THE PRIOR ART

Projection lenses for use with pixelized panels are described in various patents including Taylor, U.S. Patent No. 4,189,211, Tanaka et al., U.S. Patent No. 5,042,929, Yano et al., U.S. Patent No. 5,179,473, Moskvovich, U.S. Patent No. 5,200,861, Moskvovich, U.S. Patent No.

10 5,218,480, Iizuka et al., U.S. Patent No. 5,278,698, Betensky, U.S. Patent No. 5,313,330, and Yano, U.S. Patent No. 5,331,462.

Discussions of LCD systems can be found in Gagnon et al., U.S. Patent No. 4,425,028, Gagnon, U.S. Patent No. 4,461,542, Ledebuhr, U.S. Patent No. 4,826,311, and EPO Patent Publication No. 311,116.

15 SUMMARY OF THE INVENTION

In view of the foregoing, it is an object of the present invention to provide improved projection lenses for use with pixelized panels which simultaneously have each of the six desired properties discussed above. This object is achieved by means of a projection lens which has a focal
20 length f_0 and consists in order from its image side to its object side (i.e., from its long conjugate side to its short conjugate side) of:

(A) a first lens unit (U1) having a focal length f_1 and comprising:

- (i) a lens element (E1) having a focal length f_{E1} ; and
- (ii) at least one aspherical surface for correction of

25 distortion; and

(B) a second lens unit (U2) having a focal length f_2 and consisting in order from the image side of:

- (i) a first lens subunit (U_{2S1}) having a focal length f_{2S1} ; and
- (ii) a second lens subunit (U_{2S2}) separated from the first

30 lens subunit by an airspace (t_{S1S2}) and having a focal length f_{2S2} , said second lens subunit comprising: (a) at least one aspherical surface for

correction of spherical aberration, and (b) means for providing axial color correction for the lens system;

wherein:

- 5 $|f_1|/f_0 > 0.75;$
 $f_{E1} < 0;$
 $f_2 > 0;$
 $f_2/f_0 < 2.0;$
 $f_{S1} > 0;$
 $f_{S1}/f_0 < 1.5;$ and
10 $|f_{S2}|/f_0 > 1.5.$

In certain preferred embodiments, the lens system also satisfies some or all of the following relationships:

- $|f_{E1}|/f_0 < 1.5;$ and
15 $t_{S1S2}/f_0 > 0.1.$

- 15 In other preferred embodiments, the second lens subunit comprises in order from the image side a negative lens element, a positive lens element, and a plastic lens element having at least one aspherical surface. The plastic lens element with the aspherical surface can have a positive or negative on-axis power. This arrangement facilitates athermalization and
20 manufacture of the lens system.

- In further preferred embodiments, the semi-field of view of the projection lens is larger than 35°. In this way, the projection lens system can have an overall compact size. The clear apertures of the first and second lens units also contribute to the overall compactness of the system,
25 with the clear aperture of the first lens unit preferably being greater than the clear aperture of the second lens unit. Preferably, the clear aperture of the first lens unit is less than 0.7 times the diagonal of the pixelized panel. Examples 1-3 presented below have semi-fields of view greater than 35° and have first lens units whose maximum clear aperture is less than 0.7
30 times the diagonal of the pixelized panel for a pixelized panel having a diagonal of 12.5 inches.

Variation in the magnification of the projection lens system is preferably achieved by varying: (a) the distance between the projection lens and the pixelized panel and (b) the distance between the first and second lens units. In particular, the first and second lens units both move in the same direction relative to the pixelized panel for focusing, but at different rates so that the distance between those units changes as the lens system is focused for different magnifications.

The projection lenses of the invention are preferably designed to be substantially athermal. As discussed fully below, this is done by a combination of selecting the locations for and balancing the powers of the plastic lens elements having substantial optical power.

BRIEF DESCRIPTION OF THE DRAWINGS

Figures 1-3 are schematic side views of projection lenses constructed in accordance with the invention in combination with a pixelized panel (PP) and a Fresnel lens (FL).

Figures 4 and 5 are monochromatic optical transfer function (MTF) plots for the lens system of Figure 1 for an object (pixelized panel) height of 158 millimeters for both figures and an image (screen) height of -869 millimeters for Figure 4 and -1524 millimeters for Figure 5, i.e., Figures 4 and 5 are MTF plots for screen-to-panel magnifications of -0.182 and -0.104, respectively. The left panels of these plots show through focus data and the right panels show at focus versus frequency data. Dotted lines represent PHASE data, dashed lines represent SAG data, and solid lines represent TAN data. The focal length, f /number, and focus position for Figure 4 are 178.81, 4.00, and 0.094, respectively. The focal length, f /number, and focus position for Figure 5 are 170.48, 4.00, and -0.023, respectively.

Figure 6 is a schematic diagram showing an overall projection lens system in which the projection lens of the present invention can be used.

The foregoing drawings, which are incorporated in and constitute part of the specification, illustrate the preferred embodiments of the invention, and together with the description, serve to explain the principles

of the invention. It is to be understood, of course, that both the drawings and the description are explanatory only and are not restrictive of the invention.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

- 5 As discussed above, the lens systems of the present invention are used to image pixelized panels, e.g., large size LCD panels, in a compact set-up and, as such, must provide a wide field of view while maintaining a very good correction of distortion. The lens systems are also intended to be used over a wide range of conjugates and, therefore, must correct for
- 10 aberrations in such a way that the aberrations do not vary (increase) to any significant extent with changes in the magnification at which the lens operates.

- To achieve these goals, a wide field of view retrofocus type lens system is used. The lens system consists of two lens units -- a weaker power
- 15 first (front) lens unit (U1) on the long conjugate side of the lens system and a strong positive power second (rear) lens unit (U2) on the short conjugate side of the system. The second lens unit, in turn, consists of two lens subunits, a first (front) lens unit on the long conjugate side of the system and a second (rear) lens unit on the short conjugate side.

- 20 Important characteristics of these units and subunits are as follows:

- (1) The first unit contains an aspherical surface to provide a necessary level of correction of distortion. As discussed above, the system's distortion needs to be highly corrected for lens systems used with pixelized panels. The distortion correction of the lens systems of the present
- 25 invention is generally better than about one percent at the image, and preferably better than about 0.5 percent.
- (2) The second unit provides most of the power of the lens system. In this way, the overall length of the lens system as a whole can be reduced.
- (3) The rear subunit of the second unit includes an aspherical
- 30 surface which provides correction of spherical aberration.

(4) Both units move for focusing in the same direction but at different rates of motion to provide a very stable correction of astigmatism at various imaging conjugates.

(5) To lower the overall cost of the lens system, aspherical
5 elements are made out of optical plastic materials.

For purposes of color correction, the second lens subunit includes axial color correcting means. Various means for correcting axial color known in the art can be used. A preferred approach comprises including a negative lens element composed of a high dispersion material and at least
10 one positive lens element composed of a low dispersion material in the second lens subunit. The high and low dispersion materials can be glass or plastic.

In general terms, a high dispersion material is a material having a dispersion like flint glass and a low dispersion material is a material
15 having a dispersion like crown glass. More particularly, high dispersion materials are those having V-values ranging from 20 to 50 for an index of refraction in the range from 1.85 to 1.5, respectively, and low dispersion materials are those having V-values ranging from 35 to 75 for the same range of indices of refraction.

20 For plastic lens elements, the high and low dispersion materials can be styrene and acrylic, respectively. Other plastics can, of course, be used if desired. For example, in place of styrene, polycarbonates and copolymers of polystyrene and acrylic (e.g., NAS) having flint-like dispersions can be used. See The Handbook of Plastic Optics, U.S. Precision Lens, Inc., Cincinnati,
25 Ohio, 1983, pages 17-29.

As discussed above, the projection lenses of the invention are athermalized so that the optical performance of the system, including, in particular, the system's back focal length, does not substantially change as the projection lens is heated from room temperature to its operating
30 temperature. More specifically, the change in the back focal length is preferably less than an amount which will significantly change the

modulation transfer function (MTF) of the system, e.g., the change in the MTF at 3 cycles per millimeter should be less than about 10 percent. For the specific examples presented below, this MTF criterion corresponds to a change in the back focal length of less than about ± 0.4 millimeters. The
5 desired thermal stabilization of the lens' focus is achieved through the selection and placement in the lens of the plastic lens elements.

Ordinarily, the use of plastic lens elements has the drawback that the refractive index of plastic optical materials changes significantly with temperature. Another effect is the change in shape, i.e., expansion or
10 contraction, of plastic optical materials with temperature. This latter effect is usually less significant than the change in index of refraction.

If only low power plastic lens elements are used in a lens it is possible to achieve a balance between the thermal changes in the plastic optics and the thermal changes in the plastic or aluminum mechanical
15 components of the system, e.g., the lens barrel which is usually the major mechanical source of thermally-caused focus changes. The unrestricted use of optical plastics in a design, i.e., the ability to use at least some plastic lens elements of relatively high power, has advantages in that, since the plastic lens elements can be readily molded, non-spherical optical surfaces
20 (aspherics) can be used to maximize the capability (performance) of a particular lens design. The use of relatively high power plastic elements also leads to a lens having an overall lower cost.

If the net plastic optical power in a design is significant, then athermalization needs to be performed or the focus of the lens will change
25 significantly as the lens' temperature changes from room temperature to its operating temperature. This is especially so with projectors which must transmit significant amounts of light to a viewing screen and thus have an operating temperature significantly above room temperature.

For the projection lenses of the present invention, athermalization is
30 achieved by taking into account the location and power of the plastic lens elements, as well as the marginal ray heights at those elements.

The location of the plastic lens elements is significant in terms of the amount of temperature change the element will undergo and thus the amount of change which will occur in the element's index of refraction. In general, elements close to the light source or the image of the light source will undergo greater temperature changes. In practice, a temperature distribution in the region where the projection lens is to be located is measured with the light source and its associated illumination optics operating and those measured values are used in the design of the projection lens.

The marginal ray height at a particular plastic lens element determines, for a given thermal change, whether changes in the element's index of refraction will be significant with regard to the overall thermal stability of the lens. Elements for which the marginal ray height is small will in general have less effect on the overall thermal stability of the system than elements for which the marginal ray height is large.

Based on the foregoing considerations, athermalization is achieved by balancing the amount of negative and positive power in the plastic lens elements with the contributions of particular elements being adjusted based on the temperature change which the element is expected to undergo and the marginal ray height at the element. In practice, this athermalization procedure is incorporated into a computerized lens design program as follows. First, a ray trace is performed at a first temperature distribution and a back focal distance is calculated. The ray trace can be a paraxial ray trace for the marginal ray. Second, the same ray trace is performed at a second temperature distribution and the back focal distance is again calculated. Neither the first nor the second temperature distribution need be constant over the entire lens but can, and in the typical case does, vary from lens element to lens element. The calculated back focal distances are then constrained to a constant value as the design of the system is optimized using the lens design program.

It should be noted that the foregoing approach assumes that the

mechanical mounts for the projection lens and the pixelized panel hold the distance between the last lens surface and the panel substantially constant as the temperature of the system changes. If such an assumption is not warranted, other provisions can be made for performing the

- 5 athermalization, e.g., a measured value for the relative movement of the mechanical mounts can be included in the process or an alternate distance, e.g., the distance between the front lens surface and the panel, can be assumed to be mechanically fixed.

- Figures 1 to 3 illustrate various projection lenses constructed in
 10 accordance with the invention. Corresponding prescriptions and optical properties appear in Tables 1 to 3, respectively. HOYA or SCHOTT designations are used for the glasses employed in the lens systems. Equivalent glasses made by other manufacturers can be used in the practice of the invention. Industry acceptable materials are used for the
 15 plastic elements.

The aspheric coefficients set forth in the tables are for use in the following equation:

$$z = \frac{cy^2}{1 + [1 - (1 + k)c^2y^2]^{1/2}} + Dy^4 + Ey^6 + Fy^8 + Gy^{10} + Hy^{12} + Iy^{14}$$

- where z is the surface sag at a distance y from the optical axis of the
 20 system, c is the curvature of the lens at the optical axis, and k is a conic constant, which is zero except where indicated in the prescriptions of Tables 1-3.

- The "First-Order Data" reported in Tables 1-3 was calculated with the Fresnel lens as part of the system. The designation "a" associated with
 25 various surfaces in the tables represents an aspheric surface, i.e., a surface for which at least one of D, E, F, G, H, or I in the above equation is not zero; the designation "c" indicates a surface for which "k" in the above equation is not zero; and the designation "f" indicates a Fresnel lens. All dimensions given in the tables are in millimeters.

- 30 The tables are constructed on the assumption that light travels from

left to right in the figures. In actual practice, the viewing screen will be on the left and the pixelized panel will be on the right, and light will travel from right to left. The pixelized panel is shown in Figures 1-3 by the designation "PP" and the Fresnel lens associated with the pixelized panel is shown by the designation "FL". The Fresnel lens serves to match the light source with the entrance pupil (exit pupil in the tables) of the projection lens.

As discussed above, the projection lenses of Figures 1-3 can be focused over a large conjugate range by varying the distance between the first and second lens units in conjunction with moving the entire lens relative to the pixelized panel. As shown in Tables 1-3, the movement of the first lens unit relative to the second lens unit is in general small compared to the overall movement of the lens system relative to the pixelized panel.

The correspondence between the surface numbers of Tables 1-3 and the U1, E1, U2, U2s1, U2s2, and FL terminology discussed above is set forth in Table 4.

Table 5 summarizes various properties of the lens systems of the invention. As can be seen from this table, the lens systems of the examples satisfy the limitations set forth above regarding the focal lengths of the various lens units, subunits, and elements, as well as the limitation on the spacing (t_{s1s2}) between the subunits of the second lens unit.

Under the heading "PP22", Table 5 lists the location of the rear principal point of the second lens unit relative to the rear surface of that unit. A comparison of these values with the prescriptions of Tables 1-3 shows that the rear principal point of this unit is located well ahead of the second subunit. This distinguishes the second lens unit of the lenses of the present invention from a classical triplet for which the rear principal point would be located in the middle of the unit.

The plots of Figures 4 and 5 show the through-focus MTF on the left and the MTF at best axial focus on the right for the lens system of Figure 1

operating at screen-to-pixelized panel magnifications of -0.182 and -0.104, respectively. Data is shown for five field points, namely, on axis and 35, 70, 85 and 100 percent of maximum field height. The actual field heights at the viewing screen are shown for the right hand plots. These field heights
5 apply to both the right hand and left hand plots and are in millimeters.

The through-focus data are at the indicated spatial frequency in cycles per millimeter. Both the through-focus and best-focus data indicate tangential and sagittal (dashed curves) MTF. The modulus scale is on the left of each block and runs from zero to one. The phase of the MTF is shown
10 as a dotted curve in the best-focus plots. The scale for the phase is indicated on the right of each best-focus block and is in radian measure. All the MTF data are for a wavelength of 546.1 nanometers. The axial focus shift indicated above the best-focus plots is relative to the zero position of the through-focus plots. The best-focus plane is at the peak of the axial
15 through-focus plot.

The lens systems of Figures 2 and 3 have similar MTF plots to those of Figures 4 and 5 over the same magnification ranges. These figures illustrate that the lens systems of the present invention achieve high levels of aberration control over a wide range of magnifications as is necessary for
20 a projection lens system which is to be used with a pixelized panel.

The lenses of Figures 1-3 were designed for use with LCD panels having a diagonal of about 12.5 inches (about 320 millimeters). The panels have a pixel size of 200 microns, corresponding to over 1,000 TV lines of horizontal resolution. The images of the panels produced by the lenses of
25 the invention typically range from about 36 inches (about 900 millimeters) to about 60 inches (about 1,500 millimeters). Significantly, the lenses achieve extremely good chromatic correction to the order of a quarter pixel (50 microns) or less. This is an extremely important feature for high quality data or video projection.

30 Although specific embodiments of the invention have been described and illustrated, it is to be understood that a variety of modifications which

do not depart from the scope and spirit of the invention will be evident to persons of ordinary skill in the art from the foregoing disclosure.

TABLE 1

Surf.		Clear Aperture			
No.	Type	Radius	Thickness	Glass	Diameter
1	a	194.8286	8.00000	ACRYLIC	170.25
2	c	60.4976	109.75660		126.07
3		75.1853	10.00000	LLF1	76.48
4		136.8907	Space 1		74.90
5	Aperture stop	0.00000			73.02
6		129.0860	12.00000	SK18	72.82
7		-344.4271	21.99035		71.59
8		-108.0986	5.00000	SF10	61.54
9		205.3792	1.00000		62.92
10		201.2503	10.00000	SK18	64.24
11		∞	1.96305		69.18
12	a	-394.4647	10.00000	ACRYLIC	70.32
13	a	-100.0000	Space 2		74.84
14		∞	2.00000	ACRYLIC	320.00
15	acf	-145.1760	Image distance		320.00

Symbol Description

- a - Polynomial asphere
- c - Conic section
- f - Fresnel

Conics

Surface Number	Constant
2	-4.1664E-01
15	-1.0000E+00

Even Polynomial Aspheres

Surf.	D	E	F	G	H	I
No.						
1	-6.0946E-08	2.5026E-12	-4.2474E-16	5.0369E-20	-4.4208E-24	1.6693E-28
12	6.0712E-08	2.0076E-10	7.2384E-14	-7.5148E-17	5.4549E-20	-1.6468E-23
13	5.5349E-07	3.8742E-10	-1.5666E-14	1.3171E-17	1.3083E-20	-9.0221E-24
15	-3.5550E-09	1.5454E-14	-4.2142E-20	0.0000E+00	0.0000E+00	0.0000E+00

Variable Spaces

Focus	Space 1	Space 2	Focal Shift	Image Distance
Pos.	T(4)	T(13)		
1	25.031	227.354	-1.830	12.573
2	26.294	213.849	-1.514	12.566

TABLE 1 (continued)

First-Order Data

f/number	4.00	4.00
Magnification	-0.1818	-0.1037
Object Height	-869.00	-1524.0
Object Distance	-900.14	-1565.2
Effective Focal Length	178.81	170.48
Image Distance	12.573	12.566
Overall Length	1356.8	2009.7
Forward Vertex Distance	456.67	444.42
Barrel Length	444.10	431.85
Stop Surface Number	5	5
Distance to Stop	0.00	0.00
Stop Diameter	73.024	69.240
Entrance Pupil Distance	88.419	88.943
Exit Pupil Distance	-6246.4	-2940.9

First Order Properties of Elements

Element Number	Surface Numbers	Power	f'	lpp	l'pp
1	1 2	-0.55002E-02	-181.81	7.9311	2.4627
2	3 4	0.34935E-02	286.24	-7.4284	-13.525
3	6 7	0.67621E-02	147.88	2.0131	-5.3714
4	8 9	-0.10438E-01	-95.802	0.9875	-1.8762
5	10 11	0.31865E-02	313.82	-0.38351E-08	-6.0928
6	12 13	0.37160E-02	269.11	8.8774	2.2505
7	14 15	0.34012E-02	294.01	1.3389	-0.97909E-07

First Order Properties of Groups

Group Number	Surface Numbers	Power	f'	lpp	l'pp
1	1 4	-0.87724E-04	-11399.	-3969.1	-6275.0
2	5 13	0.38798E-02	257.74	2.1688	-49.915
3	14 15	0.34012E-02	294.01	1.3389	-0.97909E-07

First Order Properties of the Lens

Focus Position Number	Power	f'	lpp	l'pp
1	0.55926E-02	178.81	262.09	-196.91
2	0.58658E-02	170.48	249.53	-174.08

TABLE 2

Surf.	Clear Aperture			
No.	Type	Radius	Thickness	Glass Diameter
1	a	27156.6506	8.00000	ACRYLIC 156.13
2	c	61.4019	54.48984	113.69
3	a	83.5640	18.00000	ACRYLIC 98.61
4		592.1970	Space 1	95.06
5	a	106.4909	13.00000	ACRYLIC 68.99
6	a	-612.1763	18.45447	66.62
7		Aperture stop	16.00000	58.25
8	a	-79.7997	6.00000	STYRENE 61.03
9	c	277.3432	0.75000	73.29
10		230.4632	21.00000	SK5 76.92
11		-74.6603	0.50000	81.37
12	a	-104.7869	10.00000	ACRYLIC 84.05
13	a	-175.5202	Space 2	91.82
14		∞	2.00000	ACRYLIC 315.00
15	acf	-145.1760	Image distance	316.34

Symbol Description

- a - Polynomial asphere
- c - Conic section
- f - Fresnel

Conics

Surface Number	Constant
2	-2.9168E-01
9	-9.7917E+01
15	-1.0000E+00

Even Polynomial Aspheres

Surf.							
No.	D	E	F	G	H	I	
1	2.3908E-07	-3.4397E-11	2.4621E-15	1.2648E-19	-4.0977E-23	2.2303E-27	
3	-3.8129E-07	3.9533E-12	-8.4237E-15	2.2693E-18	3.7384E-22	-3.6138E-26	
5	9.8098E-07	2.6109E-10	2.0807E-14	4.2367E-17	1.6288E-20	-2.4869E-23	
6	5.9783E-07	1.3543E-12	1.7372E-13	-4.5067E-17	-4.4564E-20	-3.1331E-25	
8	-1.3838E-06	1.5573E-11	-5.1429E-13	-6.8140E-17	2.9291E-19	-2.4056E-22	
12	2.0475E-07	4.6005E-11	4.2151E-14	-7.1866E-19	-5.4839E-21	1.0257E-24	
13	3.5125E-07	7.9683E-11	9.2083E-15	-3.2327E-18	1.6141E-22	8.8822E-26	
15	-3.5550E-09	1.5454E-14	-4.2142E-20	0.0000E+00	0.0000E+00	0.0000E+00	

Variable Spaces

Focus	Space 1	Space 2	Focal	Image
Pos.	T(4)	T(13)	Shift	Distance
1	34.327	207.009	-0.823	12.493
2	35.479	193.765	-0.539	12.492

TABLE 2 (continued)

First-Order Data

f/number	4.00	4.00
Magnification	-0.1818	-0.1037
Object Height	-869.00	-1524.0
Object Distance	-900.01	-1553.1
Effective Focal Length	175.49	167.37
Image Distance	12.493	12.492
Overall Length	1322.0	1963.0
Forward Vertex Distance	422.02	409.93
Barrel Length	409.53	397.44
Stop Surface Number	7	7
Distance to Stop	0.00	0.00
Stop Diameter	57.578	54.700
Entrance Pupil Distance	80.298	80.825
Exit Pupil Distance	-2056.5	-1434.2

First Order Properties of Elements

Element Number	Surface Numbers	Power	f'	lpp	l'pp
1	1 2	-0.79984E-02	-125.03	5.3736	0.12150E-01
2	3 4	0.51188E-02	195.36	-1.9588	-13.882
3	5 6	0.53945E-02	185.38	1.2986	-7.4652
4	8 9	-0.96608E-02	-103.51	0.83532	-2.9031
5	10 11	0.10219E-01	97.852	10.229	-3.3136
6	12 13	-0.18049E-02	-554.04	-10.413	-17.442
7	14 15	0.34012E-02	294.01	1.3389	-0.97909E-07

First Order Properties of Groups

Group Number	Surface Numbers	Power	f'	lpp	l'pp
1	1 4	-0.72934E-03	-1371.1	-363.23	-589.84
2	5 13	0.46009E-02	217.35	27.600	-52.653
3	14 15	0.34012E-02	294.01	1.3389	-0.97909E-07

First Order Properties of the Lens

Focus Position Number	Power	f'	lpp	l'pp
1	0.56983E-02	175.49	240.68	-194.08
2	0.59746E-02	167.37	228.61	-171.70

TABLE 3

Surf.		Clear Aperture			
No.	Type	Radius	Thickness	Glass	Diameter
1	a	773.3177	8.00000	ACRYLIC	131.34
2	a	68.8038	Space 1		104.97
3	a	57.5756	20.00000	ACRYLIC	85.07
4	a	43000.3193	33.11847		83.24
5	Aperture stop		18.00000		54.39
6	a	-51.0808	8.00000	STYRENE	55.33
7		20188.0991	0.75000		71.92
8		399.4017	20.00000	SK18	83.61
9		-62.2385	0.50000		84.84
10		-144.3189	10.00000	ACRYLIC	91.68
11	a	-162.3311	Space 2		99.98
12		∞	2.00000	ACRYLIC	324.96
13	acf	-145.1760	Image distance		326.20

Symbol Description

- a - Polynomial asphere
- c - Conic section
- f - Fresnel

Conics

Surface

Number	Constant
13	-1.0000E+00

Even Polynomial Aspheres

Surf.								
No.	D	E	F	G	H	I		
1	2.8065E-08	-9.5802E-12	3.4911E-15	-3.8405E-19	-1.1330E-22	1.8634E-26		
2	-1.1685E-07	-1.3373E-10	5.3413E-14	-6.7212E-18	-5.2030E-21	9.4262E-25		
3	6.3109E-09	-9.3902E-12	6.7268E-14	-8.4753E-18	-1.4957E-20	5.9849E-24		
4	2.9658E-07	8.8683E-11	-2.7028E-14	-1.8565E-17	1.6503E-20	-3.2817E-24		
6	-7.5920E-07	3.0930E-10	-1.9499E-12	7.5804E-16	1.3124E-18	-1.2617E-21		
11	2.0900E-07	4.8660E-11	2.4565E-14	-1.5910E-17	5.0824E-21	-5.0813E-25		
13	-3.5550E-09	1.5454E-14	-4.2142E-20	0.0000E+00	0.0000E+00	0.0000E+00		

Variable Spaces

Focus	Space 1	Space 2	Focal	Image
Pos.	T(2)	T(11)	Shift	Distance
1	41.972	223.883	-2.707	9.996
2	38.104	217.390	-1.499	9.996

TABLE 3 (continued)

First-Order Data

f/number	4.02	4.02
Magnification	-0.1805	-0.1066
Object Height	-900.58	-1524.0
Object Distance	-1057.8	-1827.7
Effective Focal Length	203.28	201.65
Image Distance	9.9964	9.9964
Overall Length	1454.0	2213.6
Forward Vertex Distance	396.22	385.86
Barrel Length	386.22	375.86
Stop Surface Number	5	5
Distance to Stop	0.00	0.00
Stop Diameter	54.392	53.125
Entrance Pupil Distance	72.868	71.621
Exit Pupil Distance	-9386.3	-5310.9

First Order Properties of Elements

Element Number	Surface Numbers	Power	f'	lpp	l'pp
1	1 2	-0.65135E-02	-153.53	5.9007	0.52500
2	3 4	0.85660E-02	116.74	-0.17948E-01	-13.405
3	6 7	-0.11678E-01	-85.628	0.12657E-01	-5.0024
4	8 9	0.11708E-01	85.414	10.724	-1.6712
5	10 11	-0.30997E-03	-3226.1	-65.694	-73.893
6	12 13	0.34012E-02	294.01	1.3389	-0.97909E-07

First Order Properties of Groups

Group Number	Surface Numbers	Power	f'	lpp	l'pp
1	1 2	-0.65135E-02	-153.53	5.9007	0.52500
2	3 11	0.76563E-02	130.61	42.328	-87.465
3	12 13	0.34012E-02	294.01	1.3389	-0.97909E-07

First Order Properties of the Lens

Focus Position Number	Power	f'	lpp	l'pp
1	0.49192E-02	203.28	271.74	-227.27
2	0.49590E-02	201.65	265.60	-211.65

TABLE 4

Ex. No.	Front Unit (U1)	Strong Negative Element (E1)	Rear Unit (U2)	Front Subunit (U2S1)	Rear Subunit (U2S2)	Fresnel Lens (FL)
1	1 to 4	1 to 2	6 to 13	6 to 7	8 to 13	14 to 15
2	1 to 4	1 to 2	5 to 13	5 to 6	8 to 13	14 to 15
3	1 to 2	1 to 2	3 to 11	3 to 4	6 to 11	12 to 13

TABLE 5

Ex. No.	f0*	f1	fE1	f2	f2S1	f2S2	PP22	tS1S2	f3
1	168.4	-11399.00	-181.81	257.74	147.88	-347.44	-49.92	21.99	294.01
2	165.1	-1371.10	-125.03	217.35	185.38	-7102.83	-52.65	34.45	294.01
3	187.9	-153.53	-153.53	130.61	116.74	535.47	-87.47	51.12	294.01

*The f0 values listed in this table do not include the Fresnel lens (f3). The corresponding values including the Fresnel lens are 178.81, 175.49, and 203.28 for Examples 1, 2, and 3, respectively.

What is claimed is:

1. A projection lens for forming an image of an object, said projection lens having a focal length f_0 and consisting in order from its image side of:

(A) a first lens unit having a focal length f_1 and comprising:

- (i) a lens element having a focal length f_{E1} ; and
- (ii) at least one aspherical surface for correction of

distortion; and

(B) a second lens unit having a focal length f_2 and consisting in order from its image side of:

- (i) a first lens subunit having a focal length f_{2s1} ; and
- (ii) a second lens subunit separated from the first lens

subunit by an airspace and having a focal length f_{2s2} , said second lens subunit comprising: (a) at least one aspherical surface for correction of spherical aberration, and (b) means for providing axial color correction for the lens system;

wherein:

$$|f_1|/f_0 > 0.75;$$

$$f_{E1} < 0;$$

$$f_2 > 0;$$

$$f_2/f_0 < 2.0$$

$$f_{2s1} > 0;$$

$$f_{2s1}/f_0 < 1.5; \text{ and}$$

$$|f_{2s2}|/f_0 > 1.5.$$

2. A projection lens for forming an image of an object, said projection lens having a focal length f_0 and consisting in order from its image side of:

(A) a first lens unit having a focal length f_1 and comprising:

- (i) a lens element having a focal length f_{E1} ; and
- (ii) at least one aspherical surface for correction of

distortion; and

(B) a second lens unit having a focal length f_2 and consisting in order from its image side of:

- (i) a first lens subunit having a focal length f_{2s1} ; and
- (ii) a second lens subunit separated from the first lens subunit by an airspace and having a focal length f_{2s2} , said second lens subunit consisting in order from its image side of: (a) a negative lens element, (b) a positive lens element, and (c) a plastic lens element having at least one aspherical surface;

wherein:

$$\begin{aligned} |f_1|/f_0 &> 0.75; \\ f_{E1} &< 0; \\ f_2 &> 0; \\ f_2/f_0 &< 2.0; \\ f_{2s1} &> 0; \\ f_{2s1}/f_0 &< 1.5; \text{ and} \\ |f_{2s2}|/f_0 &> 1.5. \end{aligned}$$

3. The projection lens of Claim 2 wherein the plastic lens element of the second lens subunit has a positive on-axis power.

4. The projection lens of Claim 2 wherein the plastic lens element of the second lens subunit has a negative on-axis power.

5. The projection lens of Claim 2 wherein the negative lens element of the second lens subunit has a higher dispersion than the positive lens element of the second lens subunit.

6. The projection lens of Claim 1 or 2 wherein:

$$|f_{E1}|/f_0 < 1.5.$$

7. The projection lens of Claim 1 or 2 wherein:

$$t_{s1s2}/f_0 > 0.1,$$

where t_{s1s2} is the length of the airspace between the first and second lens subunits.

8. The projection lens of Claim 1 or 2 wherein the lens has a half field of view in the direction of the image of at least 35° .

9. The projection lens of Claim 1 or 2 wherein the maximum clear aperture of the first lens unit is greater than the maximum clear aperture of the second lens unit.

10. The projection lens of Claim 1 or 2 wherein the second lens unit has a rear principal point which is located ahead of the image end of the second lens subunit.

11. The projection lens of Claim 1 or 2 wherein the lens has a distortion which is less than one percent at the image.

12. The projection lens of Claim 1 or 2 wherein the object is a pixelized panel.

13. The projection lens of Claim 12 wherein the projection lens has a lateral color aberration which is less than a pixel at the object.

14. The projection lens of Claim 12 wherein the maximum clear aperture of the first lens unit is less than 0.7 times the diagonal of the pixelized panel.

15. A projection lens system for forming an image of an object, said system comprising:

(a) an illumination system comprising a light source and illumination optics which forms an image of the light source, said image of the light source being the output of the illumination system;

(b) a pixelized panel which comprises the object; and

(c) the projection lens of Claim 1 or 2.

16. The projection lens system of Claim 15 wherein the magnification of the system is changed by changing: (i) the distance between the projection lens and the pixelized panel; and (ii) the distance between the first and second lens units.

1/6

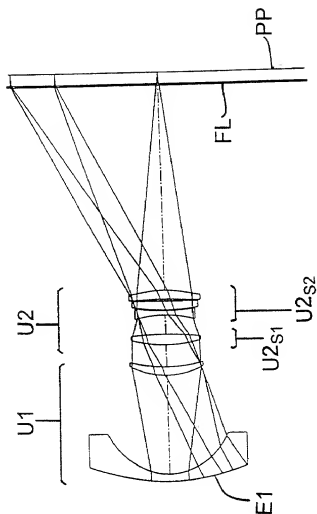


FIG. 1

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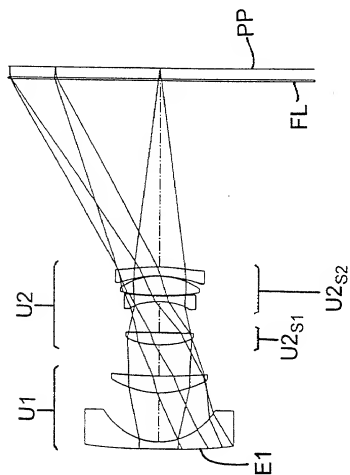


FIG. 2

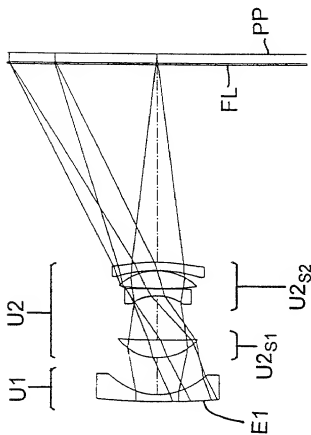


FIG. 3

4/6

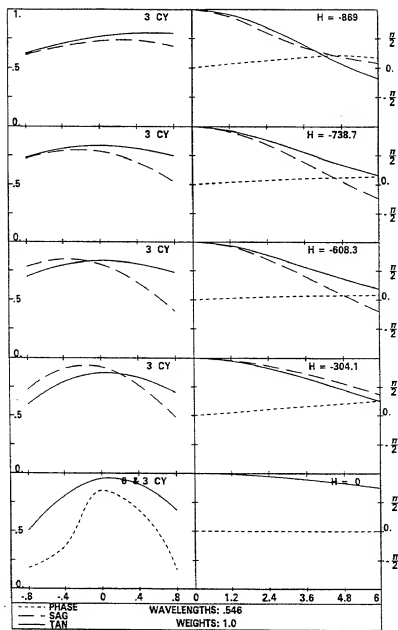


FIG. 4

5/6

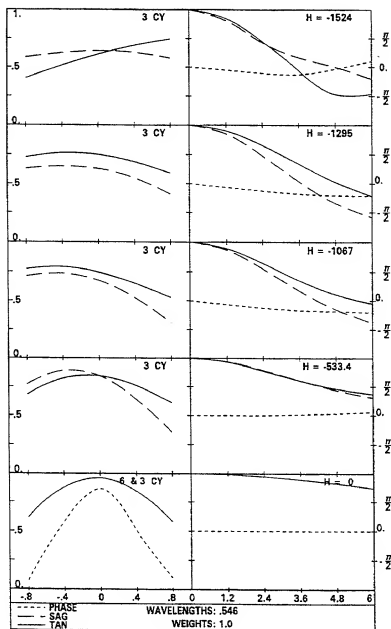


FIG. 5

6/6

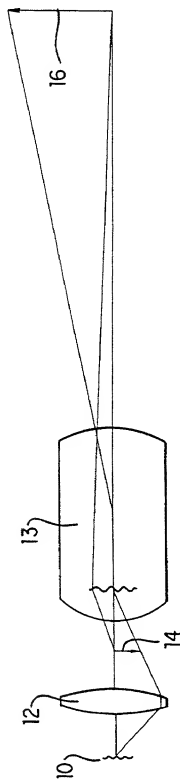


FIG. 6

DECLARATION FOR UTILITY OR DESIGN PATENT APPLICATION (37 CFR 1.63)	Attorney Docket Number	USPL-64
	First Named Inventor	MOSKOVICH, Jacob
	COMPLETE IF KNOWN	
	Application Number	
	Filing Date	
	Group Art Unit	
<input type="checkbox"/> Declaration Submitted with Initial Filing		<input type="checkbox"/> Declaration Submitted after Initial Filing (surcharge (37 CFR 1.16(e)) required)
OR		
Examiner Name		

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

WIDE FIELD OF VIEW PROJECTION LENSES FOR COMPACT PROJECTION LENS SYSTEMS EMPLOYING PIXELIZED PANELS

The specification of which

☐ is attached hereto
OR

☒ was filed on (MM/DD/YYYY) 11/10/1998 as United States Application Number or PCT International

Application Number PCT/US98/23937 and was amended on (MM/DD/YYYY) (if applicable).

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment specifically referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR 1.56.

I hereby claim foreign priority benefits under 35 U.S.C. 119(a)-(d) or 365(b) of any foreign application(s) for patent or inventor's certificate, or 365(a) of any PCT international application which designated at least one country other than the United States of America, listed below and have also identified below, by checking the box, any foreign application for patent or inventor's certificate, or of any PCT international application having a filing date before that of the application on which priority is claimed

Prior Foreign Application Number(s)	Country	Foreign Filing Date (MM/DD/YYYY)	Priority Not Claimed	Certified Copy Attached?
			<input type="checkbox"/>	YES <input type="checkbox"/>
			<input type="checkbox"/>	NO <input type="checkbox"/>
			<input type="checkbox"/>	<input type="checkbox"/>
			<input type="checkbox"/>	<input type="checkbox"/>
			<input type="checkbox"/>	<input type="checkbox"/>

☐ Additional foreign application numbers are listed on a supplemental priority data sheet PTO/SB/02B attached hereto.

I hereby claim the benefit under 35 U.S.C. 119(e) of any United States provisional application(s) listed below.

Application Number(s)	Filing Date (MM/DD/YYYY)	
60/065,308	November 13, 1997	<input type="checkbox"/> Additional provisional application numbers are listed on a supplemental priority data sheet PTO/SB/02B attached hereto.

DECLARATION - Utility or Design Patent Application

I hereby claim the benefit under 35 U.S.C. 120 of any United States application(s), or 365(c) of any PCT international application designating the United States of America, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT international application in the manner provided by the first paragraph of 35 U.S.C. 112, I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR 1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application.

U.S. Parent Application or PCT Parent Number	Parent Filing Date (MM/DD/YYYY)	Parent Patent Number (if applicable)

☐ Additional U.S. or PCT international application numbers are listed on a supplemental priority data sheet PTO/SB/02B attached hereto.

As a named inventor, I hereby appoint the following registered practitioner(s) to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith:

☐ Customer Number → Place Customer Number Bar Code Label here

OR

☒ Registered practitioner(s) name/registration number listed below

Name	Registration Number	Name	Registration Number
Maurice M. Klee	<u>30,399</u>		
Alfred L. Michaelson	<u>24,511</u>		

☐ Additional registered practitioner(s) named on supplemental Registered Practitioner Information sheet PTO/SB/02C attached hereto.

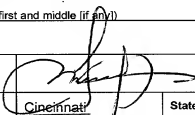
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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under 18 U.S.C. 1001 and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Name of Sole or First Inventor: ☐ A petition has been filed for this unsigned inventor

Given Name (first and middle (if any))	Family Name or Surname
<u>Jacob</u>	<u>Moskovich</u>

Inventor's Signature	Date		
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☐ Additional inventors are being named on the _____ supplemental Additional Inventor(s) sheets(s) PTO/SB/02A attached hereto.